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## (54) Optical pickup device

(57) An optical pickup device for recording and/or reproducing desired information on an information recording surface (106) of an optical disc (102) using a light beam incident on said optical disc (102) via a transparent member (104) formed on a surface of said optical disc (102) so as to be converged on the information recording surface (106), comprises a light source (110) radiating said light beam, an object lens (114) converging the light beam outgoing from said light source (110) to the information recording surface (106), and a transparent electrostriction device (120) arranged on a path of the outgoing light from said light source to the object lens (114) or a light path between the object lens (114) and the optical disc (102) and which is adapted for dividing a region transmitted through by the light beam into plural regions, the electrostriction device (120) having the thicknesses of the regions changed depending on voltages (V1, V2, V3) applied across transparent electrodes arranged on upper and lower surfaces thereof. The voltage (V1, V2, V3) applied across said regions is changed depending on the tilt of the optical recording medium for correcting the coma aberrations of the light beam on the information recording surface (106).

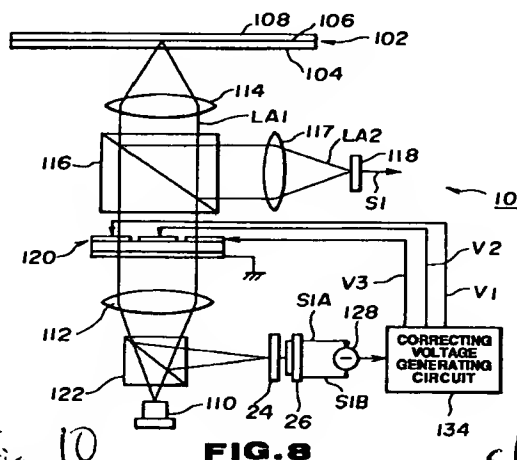


Fig. 10

FIG. 8

*- shows Seidel*

*- has 3 electrodes*  
*- not connected in series*  
*- probably could say that it would be obvious or inherent to connect in series because V1 + V3 are changed about V2 with V2 as center*

*\* teaches that ITO (indium tin oxide) is transparent*

*- Fig. 8 - shows apparatus of claim 1 excluding series set up*

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## Description

## BACKGROUND OF THE INVENTION

## 1. Field of the Invention

This invention relates to an optical pickup device for recording/reproducing information signals on or from an optical recording medium by radiating a light beam thereto from a light source, and a focusing servo device for controlling the focusing position along the optical axis of the optical pickup device.

## 2. Description of the Related Art

There has hitherto been known a magneto-optical recording medium or a phase change type optical recording medium as an optical recording medium for recording and/or reproducing information signals while a light beam from a laser light source is radiated thereto. The magneto-optical recording medium, as an example, is comprised a transparent substrate or a light-transmitting substrate, formed of, for example, a light transmitting synthetic resin, such as polycarbonate, and a magnetic layer, a dielectric layer and a surface protective layer, stacked on a major surface of the substrate. The magnetic layer, which may be a rare earth-transition metal alloy thin film, has an axis of magnetization perpendicular to the film surface and exhibits superior photomagnetic effects. Information signals may be recorded or reproduced by radiating a light beam, such as a laser beam, from the transparent substrate side.

In such optical recording medium, it is desirable to improve the recording density further in view of the fact that a data volume equal to several times to more than ten times that required for audio signals is required for recording digital video signals, and that there is a demand for a smaller size of the recording medium, such as a disc, and hence that of the player or the like even in the case of recording digital audio signals. Besides, for recording general computer data, there is an increasing demand for a smaller size or a larger recording capacity of the recording medium, in keeping up with popularization of notebook or diary size computer devices.

The information recording density on the recording medium is governed by the wavelength  $\lambda$  of the laser light and the numerical aperture NA of an object lens, such that, for increasing the recording density, it is necessary for the wavelength  $\lambda$  of the laser light to be diminished and/or for the numerical aperture NA to be increased. A so-called co-focal point detection optical system in which a pinhole is provided at a focal point of a lens at which the return light from the disc is converged, and in which the light is detected by a light receiving or detecting element is also widely used for high density reproduction.

Meanwhile, a focusing servo in such high density optical disc system has a deficiency that the defocusing tolerance becomes extremely narrow. For example, an optical pickup device making use of a light source of a short wavelength laser light, such as green or blue light, or an object lens having a larger NA value, has a smaller or shallower depth of focus. On the other hand, with an optical pickup device employing the so-called co-focal point detection system, the light volume of the detected light undergoes extremely large changes with defocusing due to its sharp depth response characteristics. In these cases, it is difficult with the conventional servo device of shifting the object lens along the optical axis, i.e. in the focusing direction, by means of an electromagnetic coil, to inhibit focusing fluctuations due to high frequency disturbances produced within the depth of focus, such as minute fluttering of the rotating disc, with respect to the resolution and bandwidths, while there lacks a device for accurately detecting focal point error signals within the depth of focus.

Meanwhile, the optical disc is subject not only to warping in the radial direction but to inundations in the circumferential direction. Besides, the optical disc is occasionally loaded in a tilted state on the recording/reproducing apparatus.

That is, in the recording/reproducing apparatus, the light spot on the information recording surface tends to be changed into the shape of a water droplet not only in the radial direction but also along the recording track(s).

If the spot shape is changed so that its long axis direction coincides with the recording track direction, inter-symbol interference is produced in the reproduced signals in the recording/reproducing apparatus, so that, if the pits are close to one another, the recording signals cannot be reproduced accurately.

Conversely, if the long axis direction is coincident with the radial direction of the optical disc, crosstalk is produced between the recording tracks to render it impossible to record the information correctly in case of a narrow track pitch.

That is, if the recording density is to be improved in the conventional recording and/or reproducing apparatus, it becomes necessary with the conventional recording/reproducing apparatus to correct the tilt of the optical disc promptly to follow up with such changes in the optical disc.

However, since these changes in the optical disc are composed of components changed with disc rotation at a frequency from tens to one hundred and tens of cycles per second (Hz), so that it is not possible with the conventional system of correcting the position of the disc in its entirety to correct the disc position unobjectionably against these changes in the optical disc.

It may also be envisaged to decrease these changes in the optical disc to improve the recording density.

However, even granting that the tilt of the optical disc may be tolerated up to  $0.6^\circ$  by employing an object lens having the numerical aperture of 0.45, the tolerable range of the tilt is diminished to  $0.25^\circ$  with the use<sup>1</sup> of an object lens having the numerical aperture of  $0.6^\circ$ , because the coma aberration is changed in proportion to the numerical aperture of the object lens multiplied thrice by itself. Consequently, an object lens having a higher numerical aperture required for improving the recording density cannot be employed, so that difficulties are met in the application of the method of reducing the disc changes to improve the recording density.

## OBJECTS AND SUMMARY OF THE INVENTION

In view of the above-described status of the art, it is a primary object of the present invention to provide an optical pickup and a focusing servo device in which focusing servo may be achieved with high accuracy even if the defocusing tolerance is reduced due to the shorter wavelength of the light source or to the high numerical aperture of the object lens as is the case when recording and/or reproducing a high density optical disc.

It is another object of the present invention to provide a disc tilt correcting device in which the tilt of the optical disc may be corrected reliably even although the recording density is improved to assure reliable reproduction of the recorded signals.

The optical pickup according to the present invention includes an optical disc for recording and/or reproducing information on or from its information recording surface, using a light beam incident on its transparent layer and converged on the signal recording surface, a light source for radiating the light beam, an object lens for converging the light beam radiated by the light source on the information recording surface, and a transparent electrostriction device interposed between the light source and the object lens or between the object lens and the optical disc for dividing the region transmitted through by the light beam into plural sub-regions. The thicknesses of these sub-regions are changed depending on voltages applied to the upper and lower transparent electrodes. The voltages applied to the sub-regions are changed depending on the tilt of the optical disc to correct the coma aberration of the light beam on the information recording surface.

With the focusing servo device according to the present invention, the focusing error within the range of the depth of focus may be detected accurately to permit fine focusing servo to assure a shorter wavelength of the light source in the high density recording medium to assure a high numerical aperture of the object lens and co-focal point detection.

By changing the thickness of the transparent electrostriction device interposed between the light source and the object lens or between the object lens and the optical disc depending on the disc tilt, it becomes possible to generate wavefront aberration by the transparent electrode device to correct wavefront aberrations caused by the disc tilt and consequently the coma aberration on the information recording surface of the optical disc.

Other objects and advantages of the present invention will become apparent from the following description.

## BRIEF DESCRIPTION OF THE DRAWINGS

Fig.1 is a schematic view showing a general arrangement of an optical disc recording/reproducing apparatus according to a first embodiment of the present invention.

Fig.2 is a perspective view of an electrostriction device employed in the embodiment of Fig.1, a portion thereof being cut away.

Fig.3 is a graph showing the relation between the applied voltage and the thickness of the electrostriction device employed in the embodiment shown in Fig.1.

Fig.4 is a graph showing depth response characteristics in the co-focal point detection in the embodiment shown in Fig.1.

Fig.5 is a graph showing focal point error detection signals in the embodiment shown in Fig.1

Fig.6 is a schematic plan view showing a light receiving pattern of a photodetector 34 when the pinhole plate 32 of the second embodiment is not employed.

Fig.7 is a schematic plan view showing a light receiving pattern of photodetectors 46, 47 when the pinhole plate 32 of the second embodiment is not employed.

Fig.8 is a schematic view showing a general arrangement of an optical disc reproducing apparatus according to a second embodiment of the present invention.

Fig.9 is a perspective view for illustrating the coma aberration produced in the embodiment shown in Fig.8.

Fig.10 is a perspective view showing a wavefront correcting plate employed in the embodiment shown in Fig.8.

Fig.11 is a graph showing the characteristics of the wavefront correcting plate.

Fig.12 is a schematic perspective view showing the wavefront aberration of the wavefront correcting plate.

Fig.13 is a front view showing light barrier plate employed in the embodiment shown in Fig.8.

Fig.14 is a front view showing a light receiving device employed in the embodiment shown in Fig.8.

Fig.15 is perspective view showing the results of correction of the wavefront aberration achieved with the embodiment shown in Fig.8.

Fig. 16 is a front view showing a wavefront correcting plate according to a third embodiment of the present invention.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to Fig. 1 showing a schematic arrangement of an optical disc recording/reproducing apparatus, an optical pickup and a focusing servo device according to a first embodiment of the present invention will be explained.

In the optical disc recording/reproducing apparatus, a laser light source, such as a semiconductor laser 11, is employed as a light source. The laser light radiated from the semiconductor laser 11 is collimated by a collimator lens 12 so as to be radiated on a recordable optical recording medium, such as a magneto-optical disc 16, by means of beam splitters 13, 14 and an object lens 15. The laser beam, radiated on the magneto-optical disc 16, is incident on and reflected by the recording layer of the magneto-optical disc 16 so as to be incident on and reflected by beam splitter 14 via object lens 15 before being incident on a photodetector 34, such as a photodiode. A pinhole plate 32 having a pinhole 33 bored therein is provided directly before the photodetector 34 for forming an optical system for co-focal point detection. A detection output from photodetector 34 is taken out via an output terminal 35.

The return light from optical disc 16 is incident via beam splitter 14 on the other beam splitter 13 so as to be converged by converging lens 41 so as to be inputted on a beam splitting prism 42. The return light incident on beam splitting prism 42 is split into a light transmitted through a beam splitting surface 42a and into a light reflected by the beam splitting surface 42a. The transmitted light is led to a pinhole 44 in a pinhole plate 43, while the reflected light is reflected by a reflecting surface 42b so as to be led to another pinhole 45 in the pinhole plate 43. Light detectors, such as photodetectors 46, 47, are arranged directly after the pinholes 44, 45, respectively. It is noted that the photodetector 46, 47 are arranged ahead and at the back of the focal point, respectively. Outputs from the photodetectors 46, 47 are differentially amplified by a differential amplifier 48, an output of which is taken out at an output terminal 49.

An electrostriction element 20 is placed between the semiconductor laser 11 as the light source and the magneto-optical disc 16 as the optical recording medium. The electrostriction element 20 is comprised of a transparent piezoelectric plate or electrostriction plate 21 of, one surface of which is coated with a transparent, electrode 22 (entire surface electrode) of, for example, so-called indium tin oxide (ITO) and the other surface of which is provided with a central transparent electrode 23 and a transparent peripheral electrode 24, as also shown in Fig. 2. The piezoelectric plate may for example be formed of PLZT or zirconium-lead titanate based ceramic, that is a  $\text{PbZrO}_3$  -  $\text{PbTiO}_3$  solid solution (so-called PZT) admixed with lanthanum (La), and is a plate of an transparent ceramic electrostriction element or a piezoelectric plate. When electrodes are fitted to both sides of the transparent piezoelectric plate 21 and an electric voltage is applied across these electrodes, the piezoelectric plate 21 is changed in thickness.

It will be seen from Fig. 3, which is a graph showing changes in thickness of the so-called PLZT device with changes in voltage applied across both electrodes of the device, that electrostriction effects in which the plate thickness is changed in accordance with a quadratic function of the impressed voltage is produced. Consequently, by applying a voltage to the central transparent electrode (central electrode) 23 of the piezoelectric plate 21 of the variable phase plate 20 which has a difference (potential difference)  $\Delta V$  from a voltage applied to the peripheral transparent electrode (peripheral electrode) of the piezoelectric plate 21, an optical phase difference may be produced.

In the embodiment of Fig. 1, a grounding voltage (GND) is applied to the entire surface electrode 22 via a terminal 27, while a predetermined constant voltage  $V$  is applied to the peripheral electrode 24 via terminal 28 and a control voltage ( $V + \Delta V$ ) from a control circuit 25 is applied to the central electrode 23 via terminal 29. The control circuit 25 performs a focusing servo operation responsive to focusing error signals from terminal 49, in such a manner that, when the focusing error is larger and outside the depth of focus, a driving coil 17 for shifting the object lens 15 along the optical axis or in the focusing direction is driven for performing a rough servo control operation and, when the focusing error is within the depth of focus, the control voltage ( $V + \Delta V$ ) is controlled to provide a phase difference between the central region and the peripheral region of the electrostriction device 20, such as the PLZT device, to effect a fine focusing servo control operation.

The principle of effecting a focal point control by providing a phase difference between the central region and the peripheral region of a light flux is explained. As disclosed in US Patent 4,861,975, entitled "Variable Focusing Optical System Employing an Electrical-Optical Material and method", affording a phase difference between the center and the periphery of a light flux is equivalent to affording a defocusing aberration within a wavelength. Therefore, the focal point position may be moved even although the position is within the depth of focus.

On the other hand, the so-called PLZT device, employed as the electrostriction device 20, is changed in thickness against the applied voltage according to a quadratic function as shown in Fig. 3 (electrostriction effect). Consequently, by controlling the voltage ( $V + \Delta V$ ) applied by control circuit 25 for affording a phase difference proportional to a focal point error between the center and a periphery of the light flux, the focal point position may be moved within the range of the depth of focus to effect a fine focusing servo control operation.

The method for accurately detecting the focal point error within the depth of focus as discussed above is explained. If the medium (disc) has a mirror surface and the pinhole 33 is small enough in size, depth response characteristics of the co-focal point detection at the photodetector 34 may be expressed by the formula

$$I(u) = (\sin(\pi u)/\pi u)^2 \quad (1)$$

where  $u$  is a normalized defocusing quantity in  $\lambda/NA^2$  and  $I(u)$  is a light intensity. When plotted along the optical axis, the formula (1) may be represented as shown in Fig. 4. The concrete value of  $\lambda/NA^2$ , as a unit for  $u$ , is  $3.12 \mu\text{m}$  for e.g. the wavelength of the laser light  $\lambda$  of  $780 \text{ nm}$  and the numerical aperture NA of the object lens of  $0.5$ . This value is that on the disc 16 and the corresponding value on the photodetector, on which the return light is incident, is  $312 \mu\text{m}$  for the numerical aperture NA of e.g.  $0.5$ , depending on the magnification factor of the converging lens.

On the other hand, the defocusing quantity  $z$  corresponding to the depth of focus, is given by

$$z = (1/2)(\lambda/NA^2) \quad (2)$$

such that the normalized defocusing quantity is equal to  $0.5$ . It is seen from Fig.4 that, for defocusing for the depth of focus of  $\pm 0.5$ , the amount of the detected light is lowered to  $40\%$ .

It will be appreciated from above that it is necessary in co-focal point detection to diminish defocusing to a value lesser than the depth of focus. The present inventors have directed their attention to detection of the focusing error signals within the depth of focus by taking advantage of the depth response of the co-focal point detection. More concretely, the difference between the outputs of the photodetectors 46, 47 arranged directly after the pinholes 44, 45 placed ahead and back of the focal point, respectively, as shown in Fig.1 is taken to effect highly accurate focal point detection even although the focal point is within the depth of focus. Taking the difference of the detection outputs is equivalent to subtracting the depth response curve of Fig.4 shifted in a horizontal direction from the original curve so that a focal point error signal having an S-shaped curve as shown in Fig.5 may be detected from output terminal 49. The curve shown in Fig.5 is equivalent to a differential output which is produced when the two pinholes 44, 45 are shifted in the fore and aft direction relative to the focal point position by an amount equal to the depth of focus, and is most suited to detection of the focal point within the range of the depth of focus.

Meanwhile, in the embodiment shown in Fig.1, the pinhole plate 32 having the pinhole 33 is arranged directly before the photodetector 34, and the pinhole plate 43 having the pinholes 44, 45 is arranged directly ahead of the photodetectors 46, 47. However, in effect, the light receiving sections of the photodetectors 34, 46, 47 may be designed as shown in Figs.6 and 7 so that the pinhole plates 32, 43 may be eliminated and signal detection of ordinary signals not employing the depth response of the co-focal point detection may be effected by the same photodetector,

Referring to Fig.6, showing a pattern of the light-receiving section of the photodetector 34 when the pinhole plate 32 is not employed, the light-receiving section is made up of a light-receiving region 34B corresponding in shape and size to the pinhole 33 and a peripheral light-receiving section therearound. The peripheral light-receiving section 34A is of such a size and shape that a beam spot SP of the return light is not deviated out of the outer rim of the light-receiving section 34A. The central light-receiving section 34B is of a diameter smaller than the diameter of the beam spot SP. In this manner, the above-described co-focal point detection signal is derived only from the central light-receiving region 34B, while the customary detection signal is produced as a sum of outputs of the light-receiving sections 34A and 34B.

Fig.7 shows a pattern of light-receiving sections of the photodetectors 46, 47 when the pinhole plate 43 is not employed, wherein the beam splitting prism 42 and the reflective surfaces 42a, 42b are indicated by imaginary lines. In Fig.7, the photodetector 46 has a light-receiving region 46C corresponding in size and shape to the pinhole 44 and a light-receiving region 46D therearound, while the photodetector 47 has a light-receiving region 47F corresponding in size and shape to the pinhole 45 and a light-receiving region 47E therearound. Consequently, if the detection outputs from these light-receiving regions 46C, 46D, 47E and 47F are indicated  $S_C$ ,  $S_D$ ,  $S_E$  and  $S_F$  the high accuracy focal point error detection signals taking advantage of the co-focal point detection for driving the above-described electrostriction element 20 may be derived from  $(S_C - S_F)$  which is a difference signal of the detection signals from the central light-receiving regions 46C and 47F, while the focal point error signal for exciting and driving the driving coil 17 for driving the object lens 15 may be derived from  $(S_C - S_D) - (S_F - S_E)$ . The lens driving focal point error signals may be designed to produce an S-shaped curve in which the amount of shift along the optical axis is of the order of 5 and the amplitude is of the order of  $-3$  to  $-4$  in terms of  $\lambda/NA^2$  as the unit.

With the above-described focusing servo, as compared to the rough servo of electro-magnetically driving the object lens 15, it is possible to cope with minute high-frequency disturbances of the order of  $\pm 1 \mu\text{m}$  due to in-plane deviations of the disc because of the high response velocity of the fine servo realized by the electrostriction element 20, so that these high-frequency disturbances may be inhibited effectively.

An optical disc recording/reproducing apparatus, to which an optical pickup device as a second embodiment of the present invention is applied, is hereinafter explained.

Fig.8 shows an optical disc recording/reproducing apparatus 101, in its entirety, for reproducing the information recorded on an optical disc 102 as a recording medium.

In the present optical disc 102, an information recording surface 106 is formed on a transparent substrate 104 and is protected by a protective film 108.

In this state, a light beam LA1 incident from the transparent substrate 104 is converged on the information recording surface 106 and the information recorded on the recording surface 106 may be reproduced based on a light beam LA2 reflected from the recording surface 106.

Thus the light beam LA1 is radiated from a laser light source 110 and collimated by a collimator lens 112 into a collimated light beam which is directed via object lens 114 on the optical disc 102.

The light beam LA2 reflected from the optical disc 102 is led via object lens 114 to a beam splitter 116 where the light beam LA2 is separated from the light beam LA1 so as to be guided via a converging lens 117 and a light-receiving element 118.

In the optical disc recording/reproducing apparatus 101, clock signals are extracted from output signals S1 of the light-receiving element 118 and signal processing is performed on the basis of these clock signals for reproducing the information recorded on the information recording surface 106.

Besides, the object lens 114 is moved vertically and horizontally based on an output signal S1 from the light-receiving element 118 for effectively avoiding tracking and focusing errors. That is, the focusing and tracking error signals are produced on the basis of the detection output of the light-receiving element 118. The object lens is driven on the basis of these focusing error signals and tracking error signals in a direction parallel to the optical axis of the object lens, i.e. in the focusing direction, and in a direction at right angles thereto, that is in the tracking direction, by an object lens driving device, not shown.

Besides, a wavefront correcting plate 120 consisting in a piezoelectric element is interposed between the collimator lens 112 and the beam splitter 116 and is driven for correcting the coma aberration.

That is, the magnitude of the coma aberration may be evaluated by a coma aberration coefficient  $W_{31}$ , with the coma aberration coefficient  $W_{31}$  on tilting of the optical disc 102 being indicated by the formula

$$W_{31} = \frac{t}{2} \frac{(N^2-1)N^2 \sin \theta \cos \theta}{(N^2 - \sin^2 \theta)^{5/2}} NA^3 = \frac{t}{2} \frac{N^2-1}{N^3} NA^3 \theta \quad (1)$$

where N is a refractive index of the transparent substrate 104, t the thickness of the transparent substrate 104,  $\theta$  the tilt of the optical disc 102 and NA the numerical aperture of the object lens 114.

That is, if the tilt has an extremely small angle, the magnitude of the coma aberration is linearly changed with the tilt.

Besides, the coma aberration itself may be expressed by the formula

$$W_{31} r^3 \cos \phi \quad (2)$$

using a pupil-shaped polar coordinate (r,  $\phi$ ). The coma aberration may be schematized as shown in Fig.9 as a wavefront on a plane of incidence of the object lens 114, wherein the radius of the pupil is normalized to 1 with the coma aberration coefficient  $W_{31}$  being indicated as 1.

Consequently, for preventing the coma aberration at the information recording surface 106, it suffices to produce the aberration shown by the formula

$$f(r, \phi) = -W_{31} r^3 \cos \phi \quad (3)$$

by means of the wavefront correcting plate 120.

With this in view, an aberration approximate to that of the formula (3) is produced by the wavefront correcting surface 120 and is used for canceling the aberration caused by the tilt of the optical disc 102 for correcting the coma aberration of the information recording surface within a practically sufficient range.

Referring to Fig.10, the wavefront correcting plate 120 is comprised of transparent electrodes 120B, 120B1 to 120B3 formed on the upper and the lower sides of a transparent crystal 120A of a perovskite structure composed of oxides of lead, lanthanum, zirconium or titanium. The area through which the light beam LA1 is transmitted is divided into three regions covered by the transparent electrodes 120B1 to 120B3.

The wavefront correcting plate 120 is maintained so that the arraying direction of the three regions is parallel to the radial direction of the optical disc. An electrical voltage corresponding to the tilt of the optical disc 102 is applied across each of these regions.

That is, with this type of the piezoelectric device, the plate thickness is changed depending on the applied voltage, as shown in Fig.11.

Consequently, when the plate 120 is inserted in a light path of the light beam LA1, the plate thickness is changed as a function of the applied voltage, so that the length of the light path of the light beam LA1 is changed for each of the transparent electrodes 120B1 to 120B3.

If, in this case, the central electrode 120B2 is maintained at a reference voltage V2, and voltages V1, V3 lower and higher than the reference voltage, respectively, are applied across the left and right electrodes 120B1 and 120B3, it

becomes possible to form a wavefront shown in Fig.12 by the wavefront correcting plate 120.

Consequently, by setting the changes in the wavefront for correcting changes in the wavefront produced on tilting of the optical disc 102, it becomes possible to correct the coma aberration on the information recording surface.

Based on this correcting principle, in the present optical disc recording/reproducing apparatus 101, a beam splitter 122 is interposed between the beam splitter 106 and the laser light source 110 for producing a split beam LA2 from the reflected light beam LA1.

The split reflected light beam LA2 is guided via a light barrier plate 124 to a light receiving device 126.

Referring to Fig.13, the light barrier plate 124 is a plate-shaped member having left and right pinholes and is maintained at a conjugate position with respect to the information recording surface 106.

Besides, the light barrier plate 124 is maintained so that the pinhole arraying direction corresponds to the arraying direction of the transparent electrodes 120B1 to 120B3 of the wavefront correcting plate 120.

In this manner, in the optical disc recording/reproducing apparatus, if the coma aberration is produced on the information recording surface 106 in the pinhole arraying direction, a coma aberration is similarly produced on the light barrier plate 124 so that the volume of light transmitted through the pinholes is changed with the amount of the coma aberration.

Referring to Fig.14, the light receiving device 126 has its light receiving surface divided in left and right regions such that the light transmitted through the pinholes of the light barrier plate 124 is incident on these regions. A subtracting circuit 128 performs a subtracting operation on output signals S1A, S1B of the light-receiving regions ARA, ARB for outputting the results of subtraction to a correction voltage generating circuit 134.

The correcting voltage generating circuit 134 maintains the central electrode 120B2 at a predetermined reference voltage V2 and, based on the results of subtraction performed by the subtracting circuit 128, generates first and second driving voltages V1, V3 changed in signal level about the reference voltage as a center, for applying the driving voltages V1, V3 to the left and right electrodes 120B1, 120B3, respectively.

By correcting the wavefront in this manner, the coma aberration may be approximately corrected, as shown in Fig.15.

However, by this correction, the wavefront aberration shown in Fig.15 may be reduced to one half in terms of the peak value and to about one-seventh in terms of a mean square value of the regions, as compared to the correction shown in Fig.9, to achieve practically sufficient results of correction.

Consequently, in the present optical disc recording/reproducing apparatus, the coma aberration may be easily corrected by simply changing over the applied voltage based on the results of detection of the coma aberration. Besides, even if the tilt of the optical disc is changed acutely, the coma aberration may be reliably corrected to follow up with these changes in the disc tilt.

Therefore, the recorded information may be reproduced reliably by a simplified arrangement even although the recording density of the optical disc is improved.

In the above arrangement, the light beam LA1 outgoing from the laser light source is collimated by a collimator lens 112 into a collimated light beam to which a predetermined wavefront aberration is applied by the wavefront correcting plate 120 before the light beam is collected by object lens 114 on the information recording surface 106.

In distinction from the light beam LA1, the reflected light beam LA2 reflected from the optical disc 102 is led via object lens 114 to the beam splitter 116 so as to be transmitted to the light receiving element 118 after reflection by the beam splitter 116.

The information recorded on the information recording surface may be reproduced on the basis of output signal S1 of the light receiving element 118.

The reflected light beam LA2 is transmitted through the wavefront correcting plate 120 and separated by the beam splitter 122 from the light beam LA1. The separated light beam is led to the light barrier plate 124 and thence to the light receiving element 126 via its pinholes so that the transmitted light volume is changed in dependence upon the coma aberration.

Output signals S1A and S1B of the light receiving element 126 are processed by a subtracting circuit 128 where the coma aberration at the optical disc 102 is detected and the driving voltages V1 to V3 are generated in the correcting voltage generating circuit 134 based on the results of detection.

In the optical disc recording/reproducing apparatus 101, the thickness of the wavefront correcting plate 120 is corrected by the driving voltages V1 to V3, while the coma aberration produced by the tilt of the optical disc is canceled by the wavefront aberration of the wavefront correcting plate 120, so that the coma aberration may be effectively prevented from being produced on the information recording surface 106.

With the above-described arrangement, albeit simplified, the coma aberration may be easily corrected by controlling the thickness of the wavefront correcting plate provided in the parallel light beam between the collimator lens and the object lens and by canceling the wavefront aberration produced by the disc tilt by the wavefront aberration of the correcting plate, so that the recorded information may be reliably reproduced even if the recording density of the optical disc is improved.

Although the correction of the coma aberration in the radial direction has been described in the second embodi-

ment, the present invention may also be applied to correction along the recording track(s) or both in the radial direction and along the recording track(s).

The disc recording/reproducing apparatus may also be so designed that, as shown in Fig.16, the piezoelectric device is divided into four regions for canceling the wavefront aberration in the radial direction and along the recording track(s) by a sole wavefront correcting plate.

Two wavefront correcting plates may also be used for correcting the coma aberration in the radial direction and along the recording track(s).

In the above-described embodiments, the wavefront correcting plate is divided into three regions for correcting the wavefront aberration. However, the correcting plate may also be divided into two regions, if practically acceptable results of correction may be achieved. The number of division of the correcting plate may also be increased.

In the above-described embodiment, the wavefront correcting plate is interposed between the collimator lens and the object lens. However, the correcting plate needs only be disposed at any selected position in the light path of the light beam LA1, such as between the object lens and the optical disc or between the collimator lens and the laser light source.

Although the reflected light beam LA2 is separated from the light beam LA1 at the back of the collimator lens for detecting the coma aberration, the light beam LA2 may be separated at various positions from the light beam LA1 for detecting the coma aberration.

Although the wavefront correcting plate is driven on the basis of the reflected light beam LA2 in the above-described embodiment, it is also possible to detect the tilt of the optical disc directly to drive the wavefront driving plate based on the results of detection.

Although the reflected light beam LA2 is led in the above embodiment to the light receiving device for reproducing the information signals based on the changes in the light volume, the present invention may also be applied to imaging an optical disc by an image pickup in reproducing the recorded information.

Above all, in a system of forming an enlarged image of the information recording surface by an image pickup, reproduction is rendered difficult if the optical disc is tilted to only a small extent. The present invention may be applied to such system for reliably reproducing the recorded information.

Although the present invention is applied in the abovedescribed embodiments to read-only disc reproducing apparatus, the present invention may also be extensively applied to an optical disc apparatus in which a light beam is applied at a predetermined timing to the information recording surface for recording and/or reproducing the desired information.

It is noted that the present invention is not limited to the above-described embodiments. For example, the electrostriction device 20 making use of the piezoelectric plate 21 may be provided at any position of the light path extending from the semiconductor laser 11 as a light source to the magneto-optical disc 16 as an optical recording medium. The recordable optical recording medium may also be a phase-change type optical disc or a card instead of the magneto-optical disc 16. The piezoelectric plate 21 of the electrostriction device 20 may be formed of a transparent material exhibiting electrostriction or piezoelectric effects instead of the PLZT. The transparent electrode 23 may also be rectangular or polygonal, instead of being circular. Besides, the entire electrode 22 on the back side of the piezoelectric plate may also be divided into a central electrode and a peripheral electrode.

The present invention provides a disc tilt correcting device in which, by interposing a piezoelectric device in the light path of the light beam and changing the thickness of the piezoelectric device for canceling the coma aberration caused by the tilt of the optical disc, it becomes possible to inhibit coma aberration on the information recording surface despite acute changes in the disc tilt to improve the recording density to assure reliable recording and/or reproduction of information signals.

## Claims

1. An optical pickup for recording and/or reproducing desired information on an information recording surface (106) of an optical disc (102) using a light beam incident on said optical disc (102) via a transparent member (104) formed on a surface of said optical disc (102) so as to be converged on said information recording surface (106), comprising

a light source (110) radiating said light beam,

an object lens (114) converging said light beam outgoing from said light source (110) to said information recording surface (106), and

a transparent electrostriction device (120) arranged on a path of the outgoing light from said light source to said object lens (114) or a light path between said object lens (114) and the optical disc (102) and adapted for dividing a region transmitted through by said light beam into plural regions, said electrostriction device (120) having the thicknesses of said regions changed depending on voltages (V1, V2, V3) applied across transparent electrodes arranged on upper and lower surfaces thereof,

said voltage (V1, V2, V3) applied across said regions being changed depending on the tilt of said optical



recording medium for correcting the coma aberrations of said light beam on said information recording surface (106).

- 5 2. The optical pickup as defined in claim 6 further comprising a beam splitter (122) for separating a light beam outgoing from said light source (110) and a return light beam from said optical disc (102), light detection means (126) for detecting the light beam separated from said beam splitter (122), and detection means (128, 134) for detecting the tilt of said optical disc (102) based on a detection output of said light detecting means (126), a detection output of said detection means (128, 134) being supplied to said electrostriction device (120).
- 10 3. The optical pickup as defined in claim 6 wherein said electrostriction device (120) comprises a piezoelectric plate (120A) and electrodes (120B, 120B1, 120B2, 120B3) arranged on both sides thereof, one of said electrodes being made up of a central electrode (120B2) and peripheral electrodes (120B1, 120B3) arranged on both sides of said central electrode (120B2).
- 15 4. The optical pickup as defined in claim 6 wherein said electrostriction device (120) comprises a piezoelectric plate and electrodes arranged on both sides thereof, one of said electrodes being formed by four divided electrodes.

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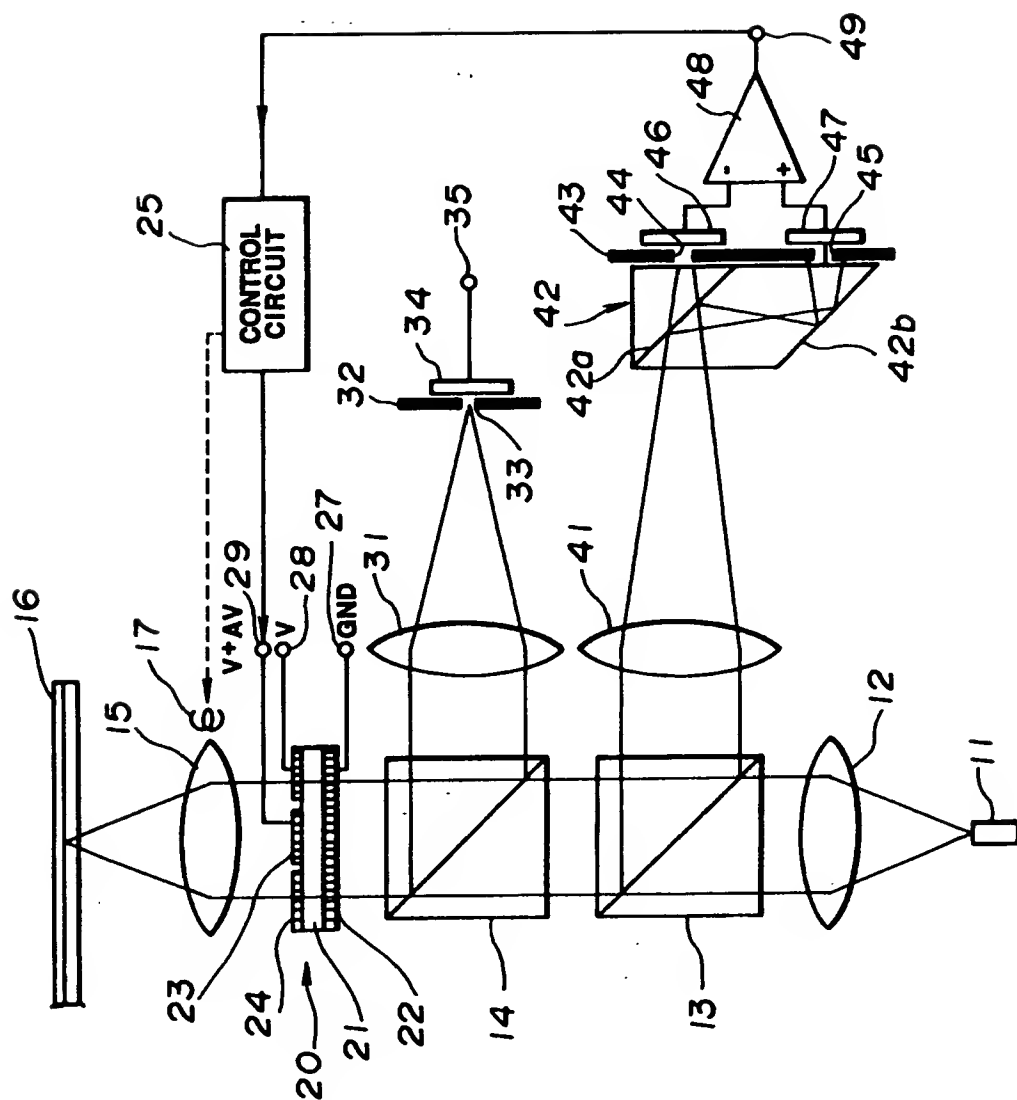
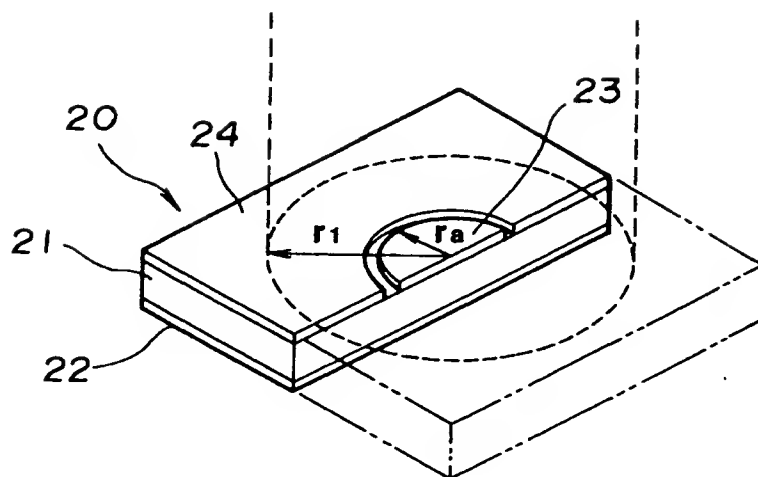
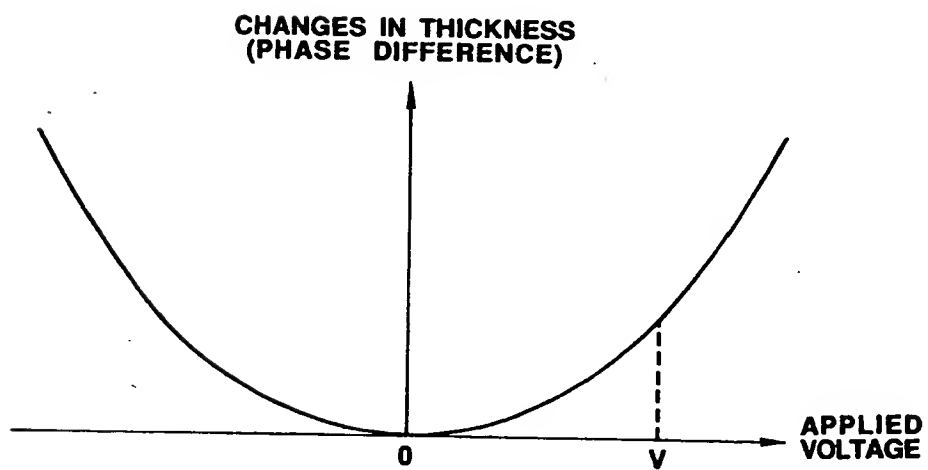


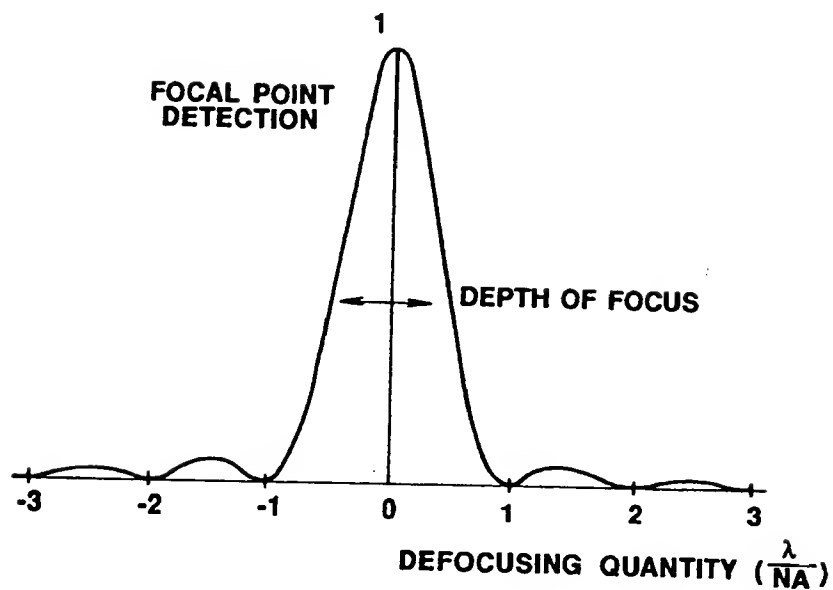
FIG.1



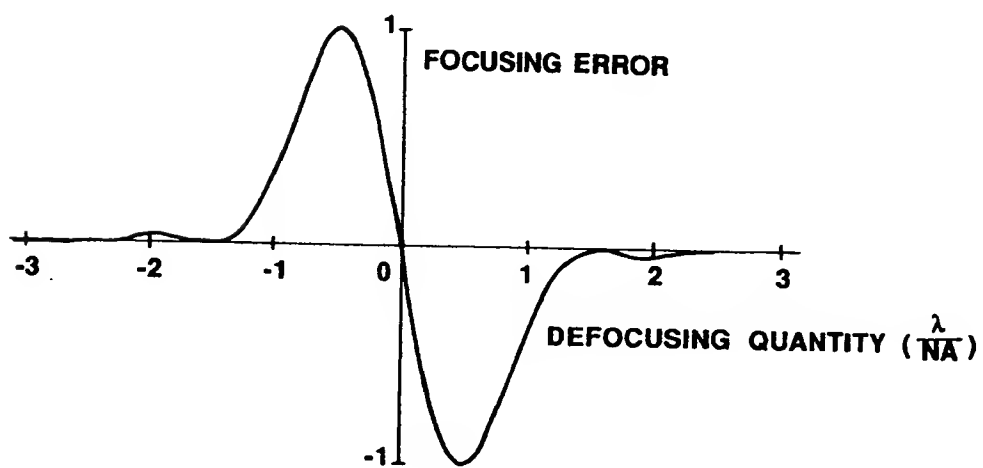
**FIG. 2**



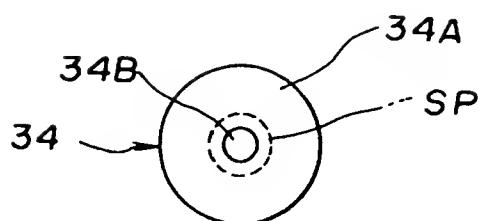
**FIG. 3**



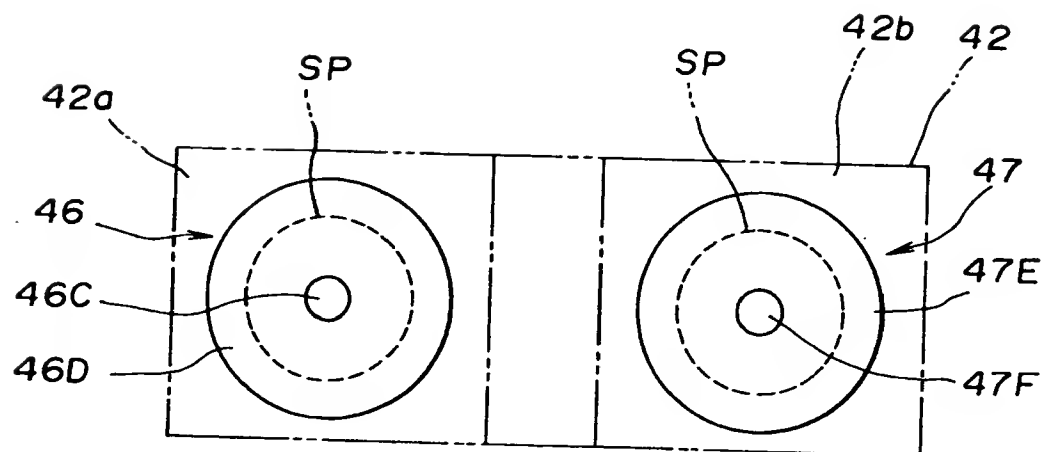
**FIG. 4**



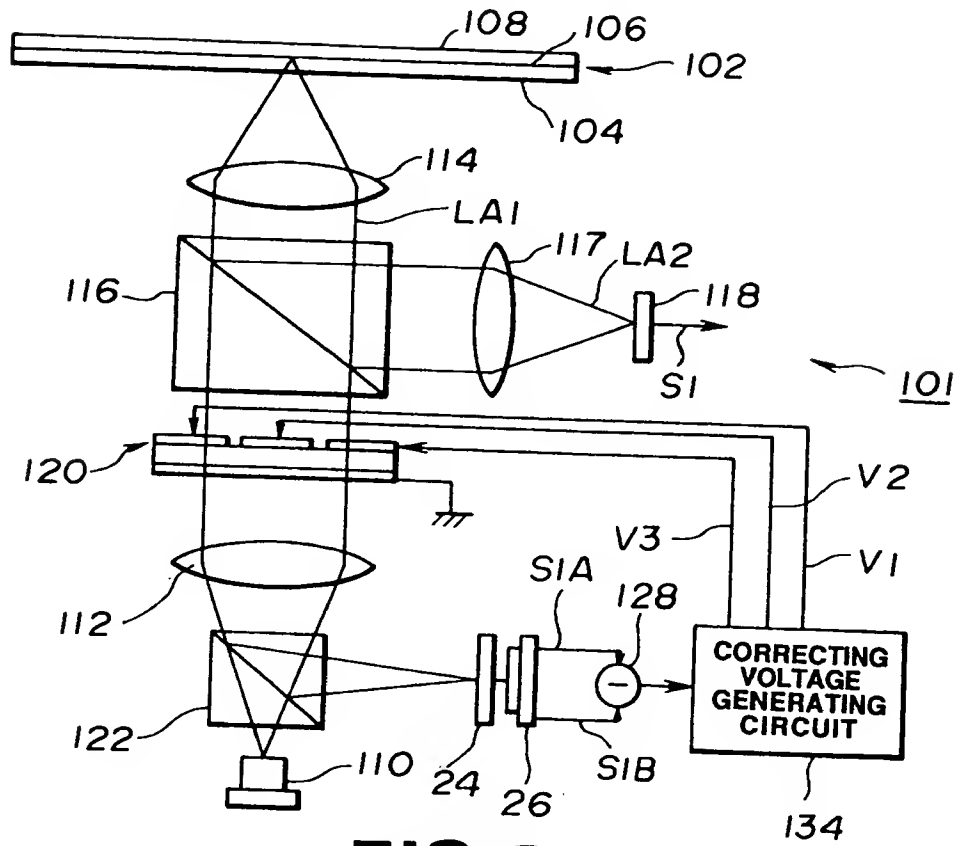
**FIG. 5**



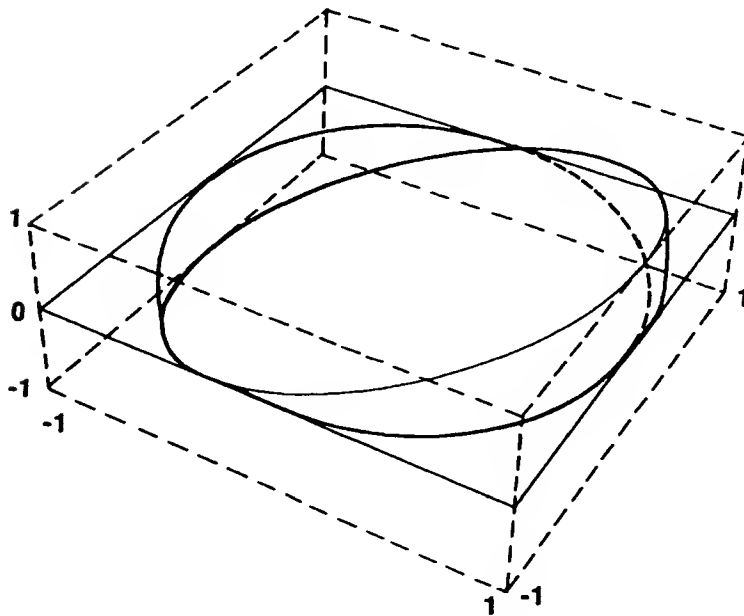
**FIG. 6**



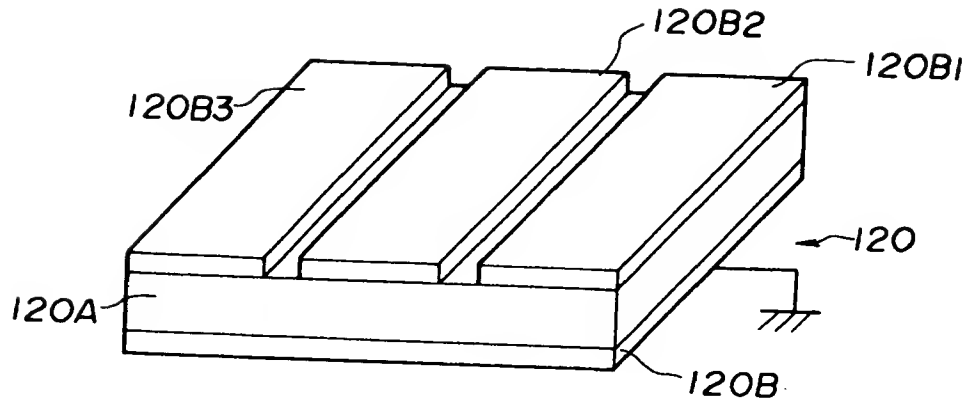
**FIG. 7**



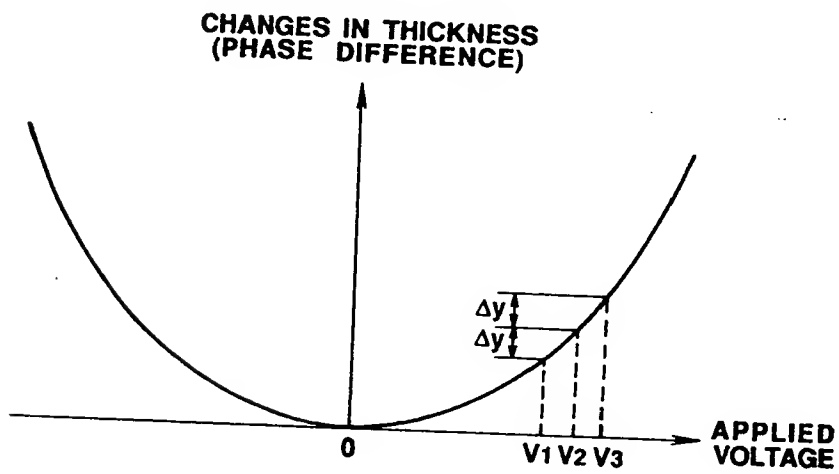
**FIG. 8**



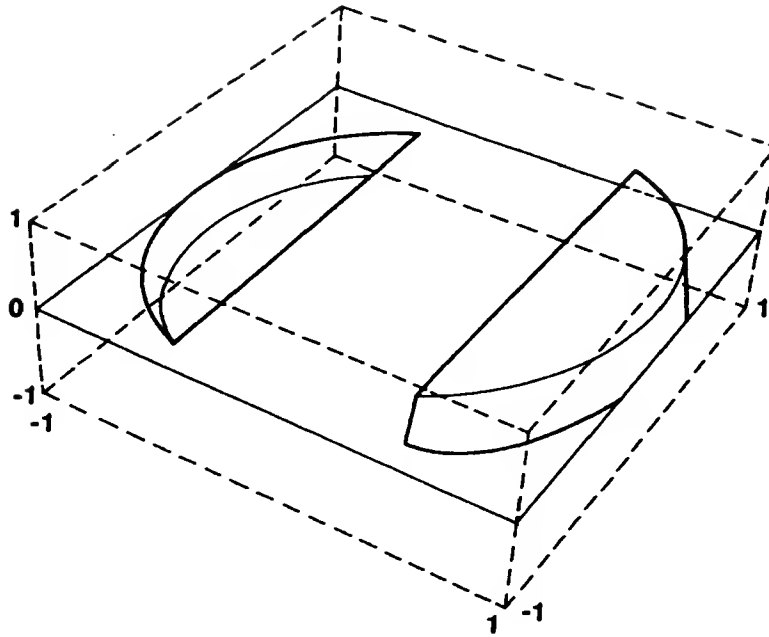
**FIG. 9**



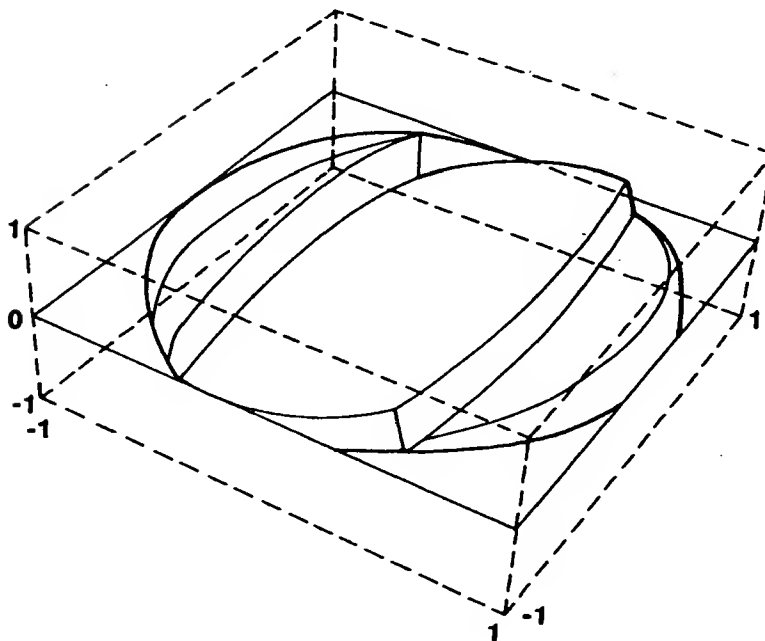
**FIG.10**



**FIG.11**

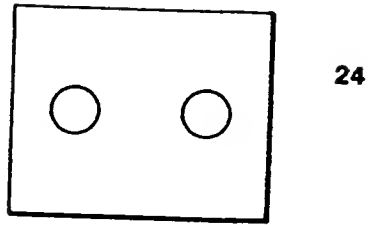


**FIG.12**

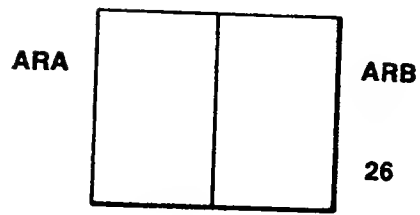


**FIG.15**

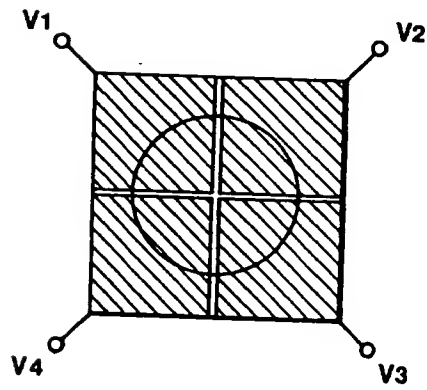




**FIG.13**



**FIG.14**



**FIG.16**



European Patent  
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# EUROPEAN SEARCH REPORT

Application Number  
EP 96 11 1456

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
D,Y	US-A-4 861 975 (KINO GORDON S ET AL) 29 August 1989 * column 3; figures 1,3 *	1-3	G11B7/09 G11B7/125 G11B7/135
Y	PATENT ABSTRACTS OF JAPAN vol. 009, no. 276 (P-402), 2 November 1985 & JP-A-60 121546 (SONY KK), 29 June 1985, * abstract *	1-3	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			G11B
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 16 September 1996	Examiner Holubov, C
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